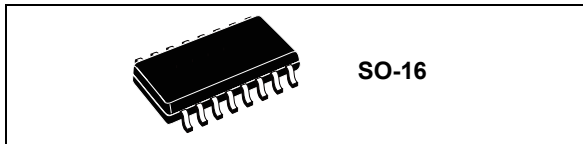


High voltage high/low-side driver

Datasheet - production data



Features

- High voltage rail up to 600 V
- dV/dt immunity ± 50 V/nsec in full temperature range
- Driver current capability: 290 mA source, 430 mA sink
- Switching times 75/35 nsec rise/fall with 1 nF load
- 3.3 V, 5 V TTL/CMOS inputs with hysteresis
- Integrated bootstrap diode
- Operational amplifier for advanced current sensing
- Comparator for fast fault protection
- Smart shutdown function
- Adjustable deadtime
- Interlocking function
- Compact and simplified layout
- Bill of material reduction

Applications

- Home appliances
- Motor drivers
 - DC, AC, PMDC and PMAC motors
 - FOC and sensorless BEMF detection systems
- Industrial applications and drives
- Induction heating
- HVAC
- Factory automation
- Power supply systems

Description

The L6390 is a full featured high voltage device manufactured with the BCD™ “offline” technology. It is a single-chip half-bridge gate driver for N-channel power MOSFETs or IGBTs. The high-side (floating) section is able to work with voltage rail up to 600 V.

Both device outputs can sink and source 430 mA and 290 mA respectively. Prevention from cross conduction is ensured by interlocking and programmable deadtime functions.

The device has dedicated input pins for each output and a shutdown pin. The logic inputs are CMOS/TTL compatible down to 3.3 V for easy interfacing with control devices. Matched delays between low-side and high-side sections guarantee no cycle distortion and allow high frequency operation.

The L6390 embeds an operational amplifier suitable for advanced current sensing in applications such as field oriented motor control or for sensorless BEMF detection. A comparator featuring advanced smartSD function is also integrated in the device, ensuring fast and effective protection against fault events like overcurrent, overtemperature, etc.

The L6390 device features also UVLO protection on both the lower and upper driving sections, preventing the power switches from operating in low efficiency or dangerous conditions.

The integrated bootstrap diode as well as all of the integrated features of this IC make the application PCB design easier, more compact and simple thus reducing the overall bill of material.

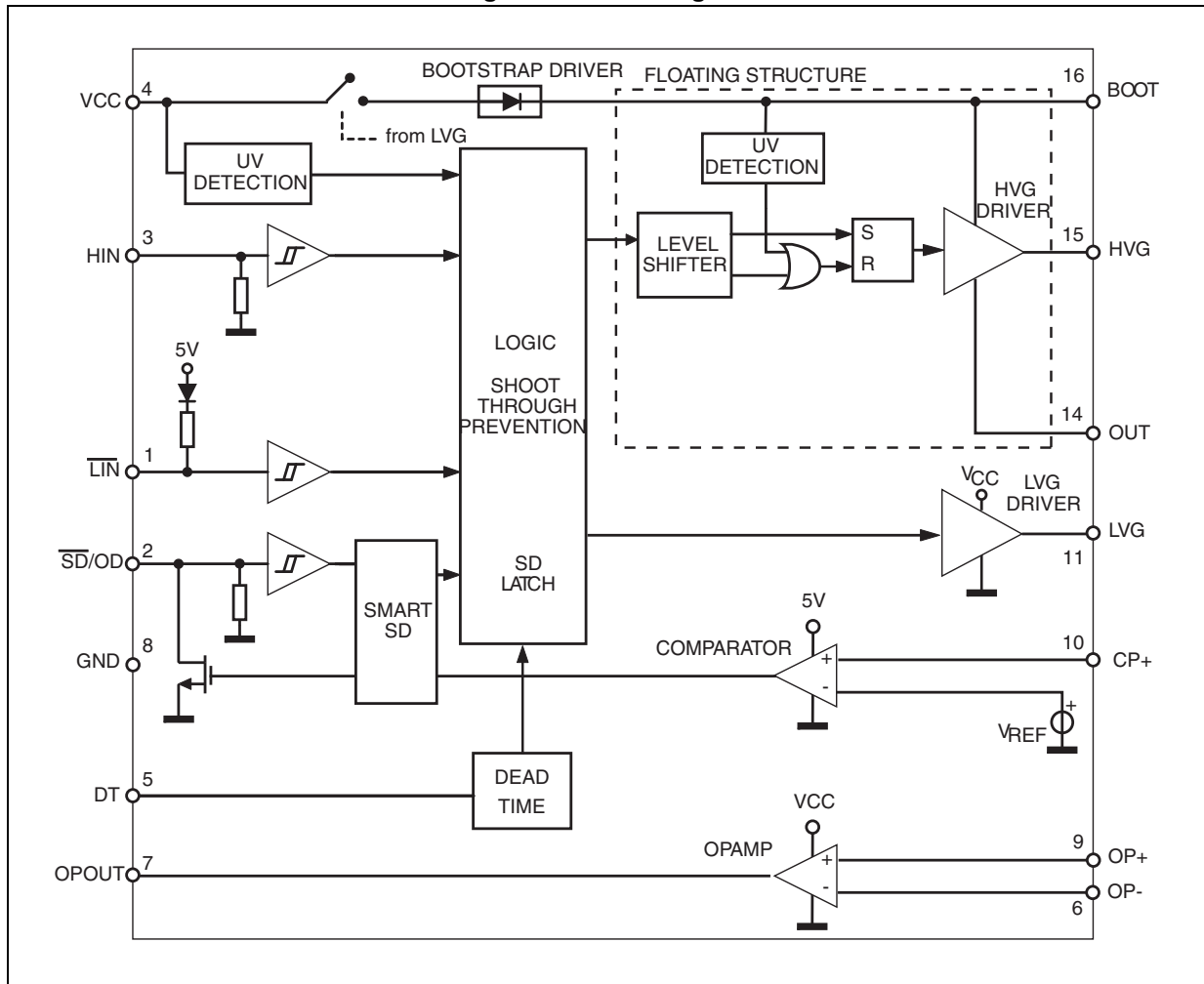
The device is available in an SO-16 tube and tape and reel packaging options.

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1 Block diagram

Figure 1. Block diagram



2 Pin connection

Figure 2. Pin connection (top view)

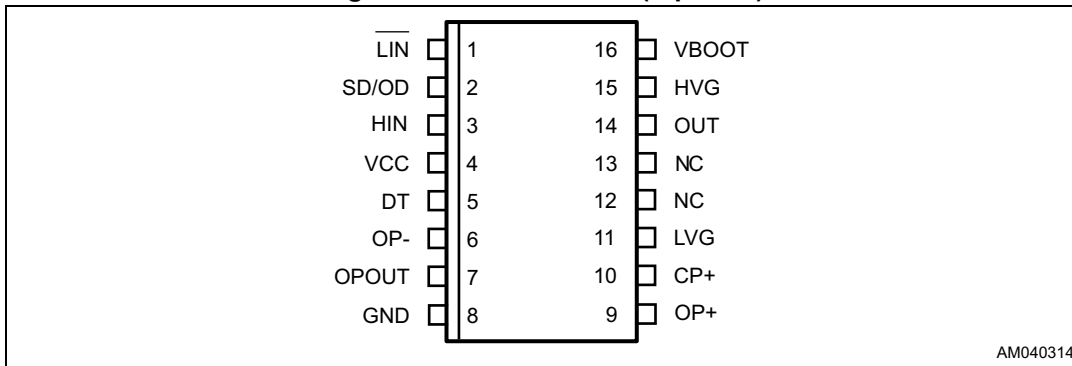


Table 1. Pin description

| Pin no. | Pin name | Type | Function |
|---------|--|------|--|
| 1 | $\overline{\text{LIN}}$ | I | Low-side driver logic input (active low) |
| 2 | $\overline{\text{SD/OD}}$ ⁽¹⁾ | I/O | Shutdown logic input (active low)/open drain (comparator output) |
| 3 | HIN | I | High-side driver logic input (active high) |
| 4 | VCC | P | Lower section supply voltage |
| 5 | DT | I | Deadtime setting |
| 6 | OP- | I | Op amp inverting input |
| 7 | OPOUT | O | Op amp output |
| 8 | GND | P | Ground |
| 9 | OP+ | I | Op amp non-inverting input |
| 10 | CP+ | I | Comparator input |
| 11 | LVG ⁽¹⁾ | O | Low-side driver output |
| 12, 13 | NC | | Not connected |
| 14 | OUT | P | High-side (floating) common voltage |
| 15 | HVG ⁽¹⁾ | O | High-side driver output |
| 16 | BOOT | P | Bootstrap supply voltage |

1. The circuit provides less than 1 V on the LVG and HVG pins (at $I_{\text{sink}} = 10 \text{ mA}$), with $V_{\text{CC}} > 3 \text{ V}$. This allows the omission of the "bleeder" resistor connected between the gate and the source of the external MOSFET normally used to hold the pin low; the gate driver assures low impedance also in SD condition.

3 Electrical data

3.1 Absolute maximum ratings

Table 2. Absolute maximum ratings

| Symbol | Parameter | Value | | Unit |
|---------------|--|-----------------|------------------|------|
| | | Min. | Max. | |
| V_{CC} | Supply voltage | - 0.3 | 21 | V |
| V_{OUT} | Output voltage | $V_{BOOT} - 21$ | $V_{BOOT} + 0.3$ | V |
| V_{BOOT} | Bootstrap voltage | - 0.3 | 620 | V |
| V_{hvg} | High-side gate output voltage | $V_{OUT} - 0.3$ | $V_{BOOT} + 0.3$ | V |
| V_{lvg} | Low-side gate output voltage | - 0.3 | $V_{CC} + 0.3$ | V |
| V_{OP+} | Op amp non-inverting input | - 0.3 | $V_{CC} + 0.3$ | V |
| V_{OP-} | Op amp inverting input | - 0.3 | $V_{CC} + 0.3$ | V |
| V_{CP+} | Comparator input voltage | - 0.3 | $V_{CC} + 0.3$ | V |
| V_i | Logic input voltage | - 0.3 | 15 | V |
| V_{od} | Open drain voltage | - 0.3 | 15 | V |
| dV_{OUT}/dt | Allowed output slew rate | - | 50 | V/ns |
| P_{tot} | Total power dissipation ($T_A = 25\text{ °C}$) | - | 800 | mW |
| T_J | Junction temperature | - | 150 | °C |
| T_{stg} | Storage temperature | -50 | 150 | °C |
| ESD | Human body model | 2 | | kV |

3.2 Thermal data

Table 3. Thermal data

| Symbol | Parameter | SO-16 | Unit |
|--------------|--|-------|------|
| $R_{th(JA)}$ | Thermal resistance junction to ambient | 120 | °C/W |

3.3 Recommended operating conditions

Table 4. Recommended operating conditions

| Symbol | Pin | Parameter | Test condition | Min. | Max. | Unit |
|----------------|---------|-------------------------|----------------------------|--------------------|------|------|
| V_{CC} | 4 | Supply voltage | - | 12.5 | 20 | V |
| $V_{BO}^{(1)}$ | 16 - 14 | Floating supply voltage | - | 12.4 | 20 | V |
| V_{OUT} | 14 | DC output voltage | - | - 9 ⁽²⁾ | 580 | V |
| f_{sw} | - | Switching frequency | HVG, LVG load $C_L = 1$ nF | - | 800 | kHz |
| T_J | - | Junction temperature | - | -40 | 125 | °C |

1. $V_{BO} = V_{BOOT} - V_{OUT}$.

2. LVG off. $V_{CC} = 12.5$ V. Logic is operational if $V_{BOOT} > 5$ V. Refer to the AN2738 for more details.

4 Electrical characteristics

4.1 AC operation

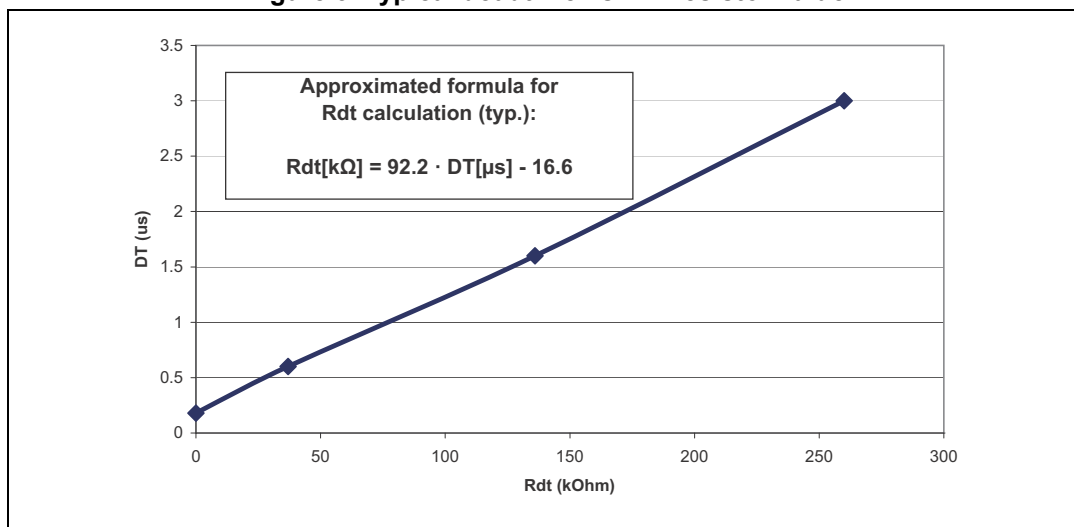
Table 5. AC operation electrical characteristics ($V_{CC} = 15\text{ V}$; $T_J = +25\text{ °C}$)

| Symbol | Pin | Parameter | Test condition | Min. | Typ. | Max. | Unit |
|-----------|--------------|--|---|------|------|------|---------------|
| t_{on} | 1 vs. 11 | High/low-side driver turn-on propagation delay | $V_{OUT} = 0\text{ V}$ $V_{BOOT} = V_{CC}$ $C_L = 1\text{ nF}$ $V_i = 0\text{ to }3.3\text{ V}$ See Figure 4 on page 12 | 50 | 125 | 200 | ns |
| t_{off} | 3 vs. 15 | High/low-side driver turn-off propagation delay | | 50 | 125 | 200 | ns |
| t_{sd} | 2 vs. 11, 15 | Shutdown to high/low-side driver propagation delay | | 50 | 125 | 200 | ns |
| t_{isd} | - | Comparator triggering to high/low-side driver turn-off propagation delay | Measured applying a voltage step from 0 V to 3.3 V to pin CP+. | 50 | 200 | 250 | ns |
| MT | - | Delay matching, HS and LS turn-on/off | - | - | 30 | ns | |
| DT | 5 | Deadtime setting range ⁽¹⁾ | $R_{DT} = 0, C_L = 1\text{ nF}$ | 0.1 | 0.18 | 0.25 | μs |
| | | | $R_{DT} = 37\text{ k}\Omega, C_L = 1\text{ nF}, C_{DT} = 100\text{ nF}$ | 0.48 | 0.6 | 0.72 | μs |
| | | | $R_{DT} = 136\text{ k}\Omega, C_L = 1\text{ nF}, C_{DT} = 100\text{ nF}$ | 1.35 | 1.6 | 1.85 | μs |
| | | | $R_{DT} = 260\text{ k}\Omega, C_L = 1\text{ nF}, C_{DT} = 100\text{ nF}$ | 2.6 | 3.0 | 3.4 | μs |
| MDT | - | Matching deadtime ⁽²⁾ | $R_{DT} = 0, C_L = 1\text{ nF}$ | - | - | 80 | ns |
| | | | $R_{DT} = 37\text{ k}\Omega, C_L = 1\text{ nF}, C_{DT} = 100\text{ nF}$ | - | - | 120 | ns |
| | | | $R_{DT} = 136\text{ k}\Omega, C_L = 1\text{ nF}, C_{DT} = 100\text{ nF}$ | - | - | 250 | ns |
| | | | $R_{DT} = 260\text{ k}\Omega, C_L = 1\text{ nF}, C_{DT} = 100\text{ nF}$ | - | - | 400 | ns |
| t_r | 11, 15 | Rise time | $C_L = 1\text{ nF}$ | - | 75 | 120 | ns |
| t_f | | Fall time | $C_L = 1\text{ nF}$ | - | 35 | 70 | ns |

1. See [Figure 3](#).

2. $MDT = |DT_{LH} - DT_{HL}|$ see [Figure 6 on page 13](#).

Figure 3. Typical deadtime vs. DT resistor value



4.2 DC operation

Table 6. DC operation electrical characteristics ($V_{CC} = 15\text{ V}$; $T_J = +25\text{ }^\circ\text{C}$)

| Symbol | Pin | Parameter | Test condition | Min. | Typ. | Max. | Unit |
|--|-----|---|--|------|------|------|---------------|
| Low supply voltage section | | | | | | | |
| V_{CC_hys} | 4 | V_{CC} UV hysteresis | - | 1200 | 1500 | 1800 | mV |
| V_{CC_thON} | | V_{CC} UV turn-ON threshold | - | 11.5 | 12 | 12.5 | V |
| V_{CC_thOFF} | | V_{CC} UV turn-OFF threshold | - | 10 | 10.5 | 11 | V |
| I_{QCCU} | | Undervoltage quiescent supply current | $V_{CC} = 10\text{ V}$ $\overline{SD} = 5\text{ V}$; $\overline{LIN} = 5\text{ V}$; $HIN = GND$; $R_{DT} = 0\ \Omega$; $CP+ = OP+ = GND$; $OP- = 5\text{ V}$ | 90 | 120 | 150 | μA |
| I_{QCC} | | Quiescent current | $V_{CC} = 15\text{ V}$ $\overline{SD} = 5\text{ V}$; $\overline{LIN} = 5\text{ V}$; $HIN = GND$; $R_{DT} = 0\ \Omega$; $CP+ = OP+ = GND$; $OP- = 5\text{ V}$ | 300 | 720 | 1000 | μA |
| V_{ref} | - | Internal reference voltage | - | 500 | 540 | 580 | mV |
| Bootstrapped supply voltage section⁽¹⁾ | | | | | | | |
| V_{BO_hys} | 16 | V_{BO} UV hysteresis | - | 1200 | 1500 | 1800 | mV |
| V_{BO_thON} | | V_{BO} UV turn-ON threshold | - | 11.1 | 11.5 | 12.1 | V |
| V_{BO_thOFF} | | V_{BO} UV turn-OFF threshold | - | 9.8 | 10 | 10.6 | V |
| I_{QBOU} | | Undervoltage V_{BO} quiescent current | $V_{BO} = 9\text{ V}$ $\overline{SD} = 5\text{ V}$; \overline{LIN} and $HIN = 5\text{ V}$; $R_{DT} = 0\ \Omega$; $CP+ = OP+ = GND$; $OP- = 5\text{ V}$ | 30 | 70 | 110 | μA |
| I_{QBO} | | V_{BO} quiescent current | $V_{BO} = 15\text{ V}$ $\overline{SD} = 5\text{ V}$; \overline{LIN} and $HIN = 5\text{ V}$; $R_{DT} = 0\ \Omega$; $CP+ = OP+ = GND$; $OP- = 5\text{ V}$ | 30 | 150 | 240 | μA |
| I_{LK} | - | High voltage leakage current | $V_{hvg} = V_{OUT} = V_{BOOT} = 600\text{ V}$ | - | - | 10 | μA |
| $R_{DS(on)}$ | - | Bootstrap driver on-resistance ⁽²⁾ | LVG ON | - | 120 | - | Ω |

Table 6. DC operation electrical characteristics ($V_{CC} = 15\text{ V}$; $T_J = +25\text{ }^\circ\text{C}$) (continued)

| Symbol | Pin | Parameter | Test condition | Min. | Typ. | Max. | Unit |
|--------------------------------|---------|---|--|------|------|------|------------------|
| Driving buffers section | | | | | | | |
| I_{so} | 11, 15 | High/low-side source short-circuit current | $V_{IN} = V_{ih} (t_p < 10\ \mu\text{s})$ | 200 | 290 | - | mA |
| I_{si} | | High/low-side sink short-circuit current | $V_{IN} = V_{il} (t_p < 10\ \mu\text{s})$ | 250 | 430 | - | mA |
| Logic inputs | | | | | | | |
| V_{il} | 1, 2, 3 | Low level logic threshold voltage | - | 0.8 | - | 1.1 | V |
| V_{ih} | | High level logic threshold voltage | - | 1.9 | - | 2.25 | V |
| V_{il_S} | 1, 3 | Single input voltage | \overline{LIN} and HIN connected together and floating | - | - | 0.8 | V |
| I_{HINh} | 3 | HIN logic "1" input bias current | HIN = 15 V | 110 | 175 | 260 | μA |
| I_{HINl} | | HIN logic "0" input bias current | HIN = 0 V | - | - | 1 | μA |
| I_{LINl} | 1 | \overline{LIN} logic "0" input bias current | $\overline{LIN} = 0\text{ V}$ | 3 | 6 | 20 | μA |
| I_{LINh} | | \overline{LIN} logic "1" input bias current | $\overline{LIN} = 15\text{ V}$ | - | - | 1 | μA |
| I_{SDh} | 2 | \overline{SD} logic "1" input bias current | $\overline{SD} = 15\text{ V}$ | 10 | 40 | 100 | μA |
| I_{SDl} | | \overline{SD} logic "0" input bias current | $\overline{SD} = 0\text{ V}$ | - | - | 1 | μA |
| R_{PD_SD} | 2 | \overline{SD} input pull-down resistor | $\overline{SD} = 15\text{ V}$ | 150 | 375 | 1500 | $\text{k}\Omega$ |

1. $V_{BO} = V_{BOOT} - V_{OUT}$.

2. R_{DSON} is tested in the following way: $R_{DSON} = [(V_{CC} - V_{BOOT1}) - (V_{CC} - V_{BOOT2})] / [I_1(V_{CC}, V_{BOOT1}) - I_2(V_{CC}, V_{BOOT2})]$ where I_1 is the pin 16 current when $V_{BOOT} = V_{BOOT1}$, I_2 when $V_{BOOT} = V_{BOOT2}$.

Table 7. Op amp characteristics⁽¹⁾ ($V_{CC} = 15\text{ V}$, $T_J = +25\text{ °C}$)

| Symbol | Pin | Parameter | Test condition | Min. | Typ. | Max. | Unit |
|-------------|------|-----------------------------------|--|------|------|------------|------------|
| V_{io} | 6, 9 | Input offset voltage | $V_{ic} = 0\text{ V}$, $V_o = 7.5\text{ V}$ | - | - | 6 | mV |
| I_{io} | | Input offset current | $V_{ic} = 0\text{ V}$, $V_o = 7.5\text{ V}$ | - | 4 | 40 | nA |
| I_{ib} | | Input bias current ⁽²⁾ | | - | 100 | 200 | nA |
| V_{icm} | | Input common mode voltage range | - | 0 | - | $V_{CC}-4$ | V |
| V_{OPOUT} | 7 | Output voltage swing | OPOUT = OP-; no load | 0.07 | - | $V_{CC}-4$ | V |
| I_o | | Output short-circuit current | Source, $V_{id} = +1$; $V_o = 0\text{ V}$ | 16 | 30 | - | mA |
| | | | Sink, $V_{id} = -1$; $V_o = V_{CC}$ | 50 | 80 | - | mA |
| SR | - | Slew rate | $V_i = 1 \div 4\text{ V}$; $C_L = 100\text{ pF}$; unity gain | 2.5 | 3.8 | - | V/ μ s |
| GBWP | - | Gain bandwidth product | $V_o = 7.5\text{ V}$ | 8 | 12 | - | MHz |
| A_{vd} | - | Large signal voltage gain | $R_L = 2\text{ k}\Omega$ | 70 | 85 | - | dB |
| SVR | - | Supply voltage rejection ratio | vs. V_{CC} | 60 | 75 | - | dB |
| CMRR | - | Common mode rejection ratio | - | 55 | 70 | - | dB |

1. The operational amplifier is disabled when V_{CC} is in UVLO condition.
2. Input bias current flows out the IC leads.

Table 8. Sense comparator characteristics⁽¹⁾ ($V_{CC} = 15\text{ V}$, $T_J = +25\text{ °C}$)

| Symbol | Pin | Parameter | Test condition | Min. | Typ. | Max. | Unit |
|---------------|-----|-------------------------------------|--|------|------|------|------------|
| I_{ib} | 10 | Input bias current | $V_{CP+} = 1\text{ V}$ | - | - | 1 | μ A |
| V_{OL} | 2 | Open drain low level output voltage | $I_{OD} = -3\text{ mA}$ | - | - | 0.5 | V |
| R_{ON_OD} | 2 | Open drain ON resistor | - | - | 125 | 167 | Ω |
| t_{d_comp} | - | Comparator delay | \overline{SD}/OD pulled to 5 V through 100 k Ω resistor | - | 90 | 130 | ns |
| SR | 2 | Slew rate | $C_L = 180\text{ pF}$; $R_{pu} = 5\text{ k}\Omega$ | - | 60 | - | V/ μ s |

1. The comparator is disabled when V_{CC} is in UVLO condition.

5 Timing and waveforms definitions

Figure 4. Propagation delay timing definition

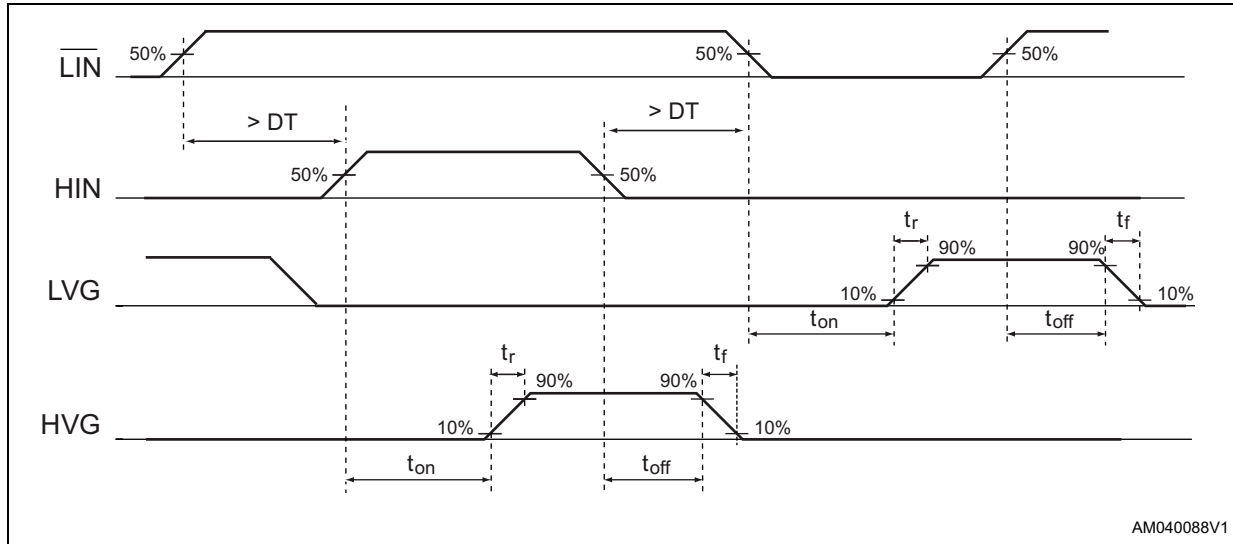


Figure 5. Dead time and interlocking timing definitions

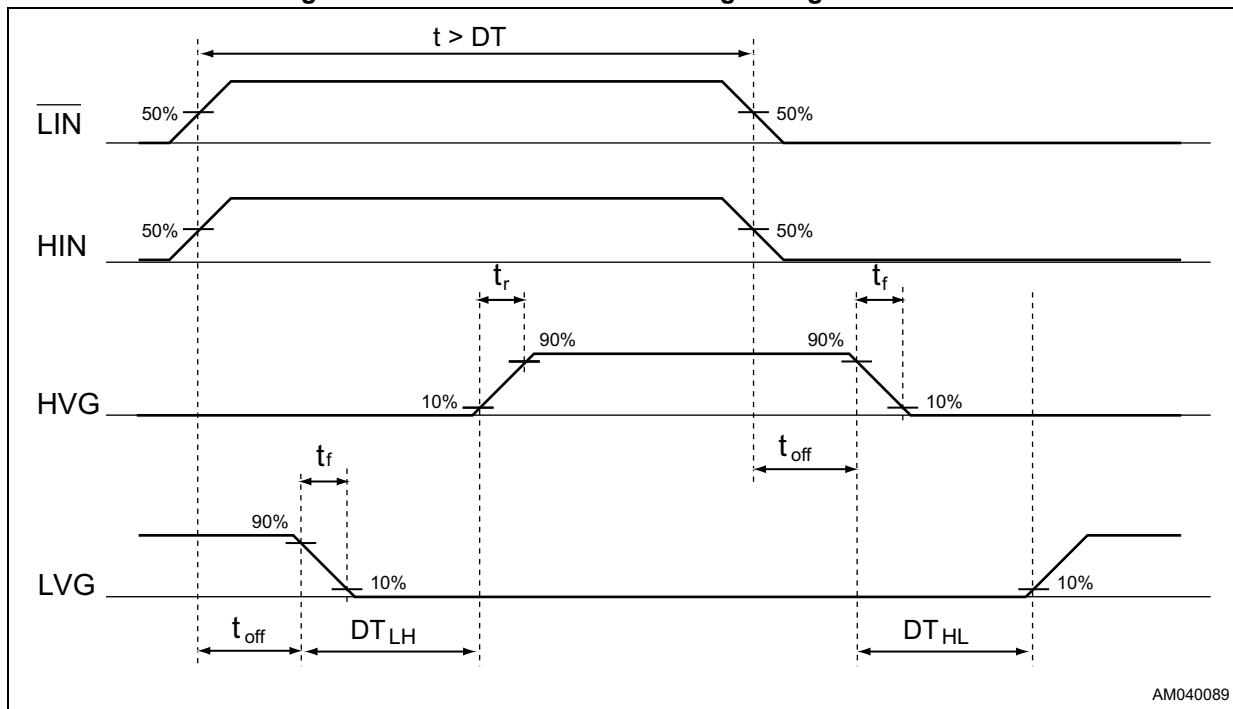
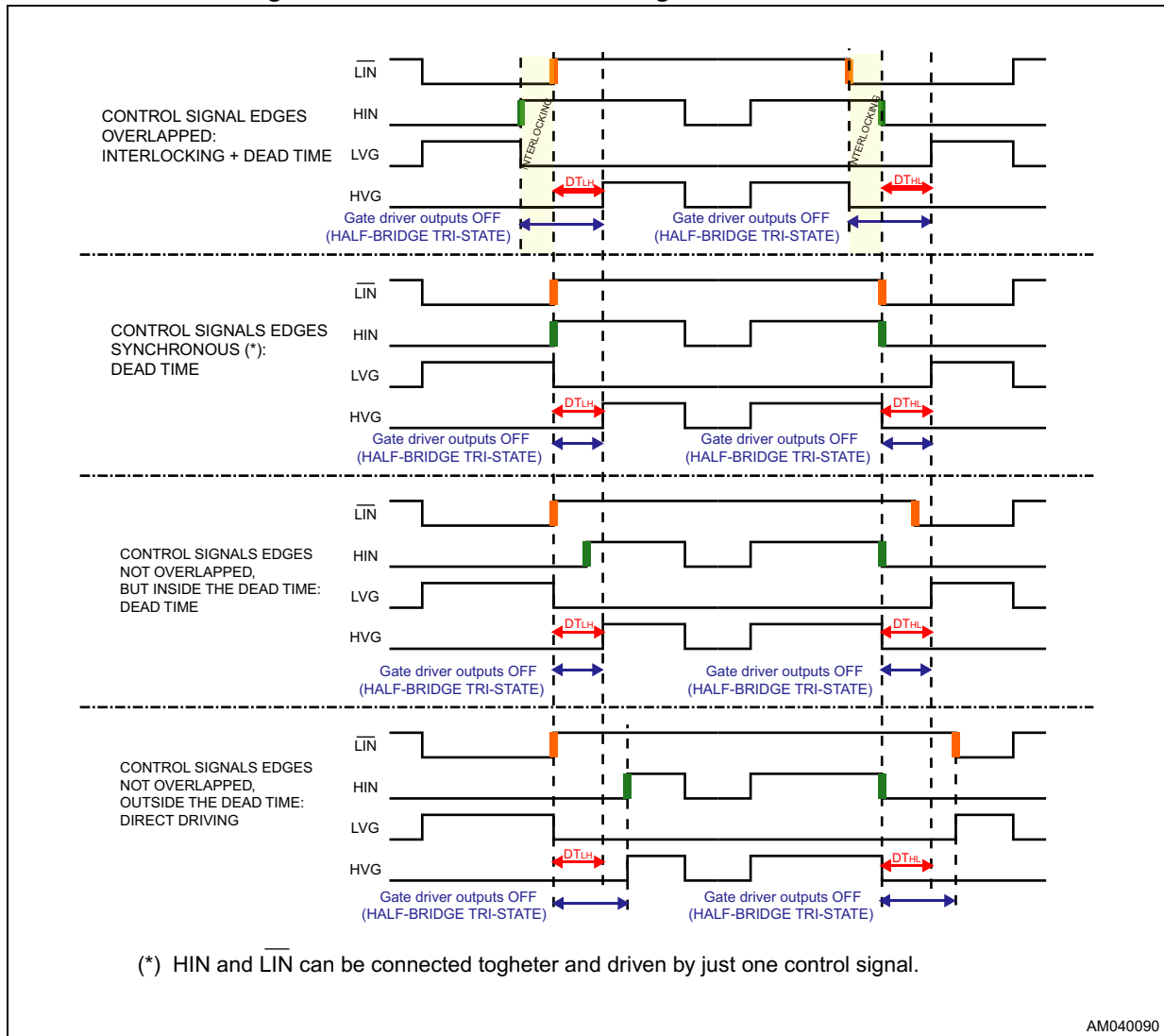


Figure 6. Deadtime and interlocking waveforms definition



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6 Input logic

Input logic is provided with an interlocking circuitry which avoids cross-conduction in case of wrong signals on LIN and HIN tries to turn-on both LVG and HVG outputs at the same times. In addition, to prevent cross conduction of the external MOSFETs, after each output is turned off, the other output cannot be turned on before a certain amount of time (DT) (see [Figure 5: Dead time and interlocking timing definitions](#)).

Table 9. Truth table

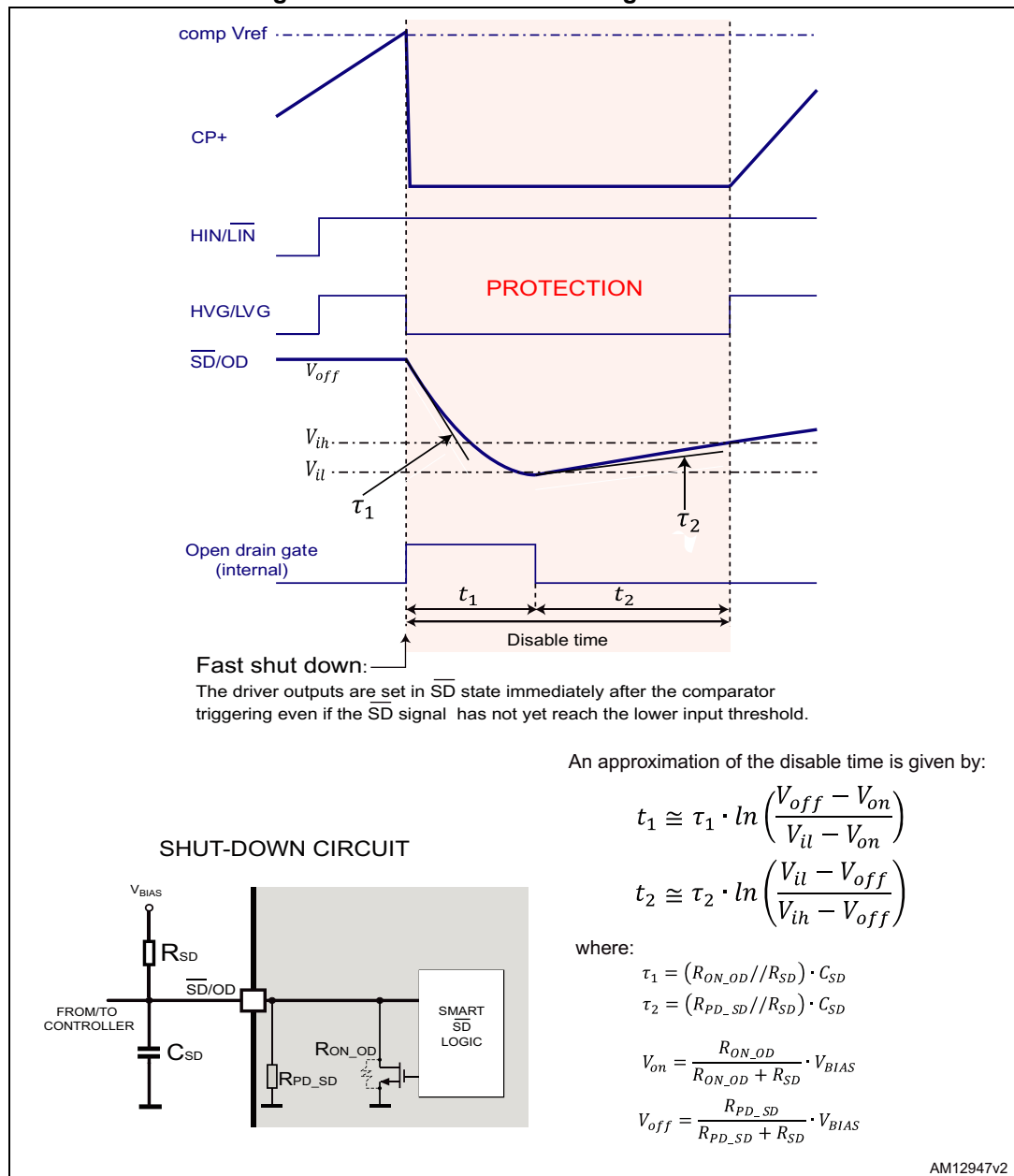
| Input | | | Output | |
|------------------------|-------------------------|------------------|--------|-----|
| $\overline{\text{SD}}$ | $\overline{\text{LIN}}$ | HIN | LVG | HVG |
| L | X ⁽¹⁾ | X ⁽¹⁾ | L | L |
| H | H | L | L | L |
| H | L | H | L | L |
| H | L | L | H | L |
| H | H | H | L | H |

1. X: don't care.

7 Smart shutdown function

The L6390 device integrates a comparator committed to the fault sensing function. The comparator has an internal voltage reference V_{ref} connected to the inverting input, while the non-inverting input is available on the pin 10. The comparator input can be connected to an external shunt resistor in order to implement a simple overcurrent detection function. The output signal of the comparator is fed to an integrated MOSFET with the open drain output available on the pin 2, shared with the \overline{SD} input. When the comparator triggers, the device is set in shutdown state and both its outputs are set to low level leaving the half-bridge in tristate.

Figure 7. Smart shutdown timing waveforms

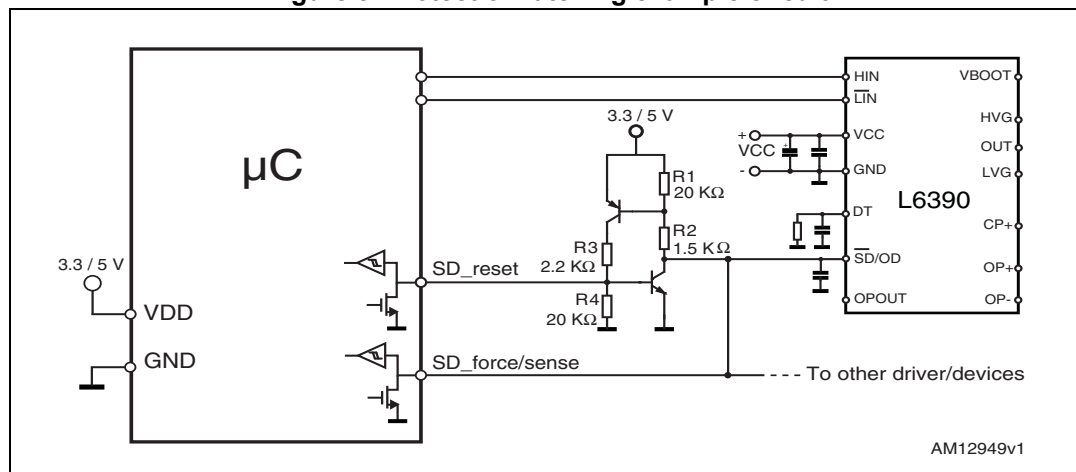


In common overcurrent protection architectures the comparator output is usually connected to the SD input and an RC network is connected to this SD/OD line in order to provide a monostable circuit, which implements a protection time that follows the fault condition. Differently from the common fault detection systems, the L6390 smart shutdown architecture allows immediate turn-off of the outputs of the gate driver in the case of fault, by minimizing the propagation delay between the fault detection event and the actual output switch-off. In fact, the time delay between the fault detection and the output turn-off is no longer dependent on the value of the external RC network connected to the SD/OD pin. In the smart shutdown circuitry the fault signal has a preferential path which directly switches off the outputs after the comparator triggering. At the same time the internal logic turns on the open drain output and holds it on until the SD voltage goes below the SD logic input lower threshold. When such threshold is reached, the open drain output is turned off, allowing the external pull-up to recharge the capacitor. The driver outputs restart following the input pins as soon as the voltage at the SD/OD pin reaches the higher threshold of the SD logic input. The smart shutdown system provides the possibility to increase the time constant of the external RC network (that determines the disable time after the fault event) up to very large values without increasing the delay time of the protection.

Any external signal provided to the SD pin is not latched and can be used as control signal in order to perform, for instance, PWM chopping through this pin. In fact when a PWM signal is applied to the SD input and the logic inputs of the gate driver are stable, the outputs switch from the low level to the state defined by the logic inputs and vice versa.

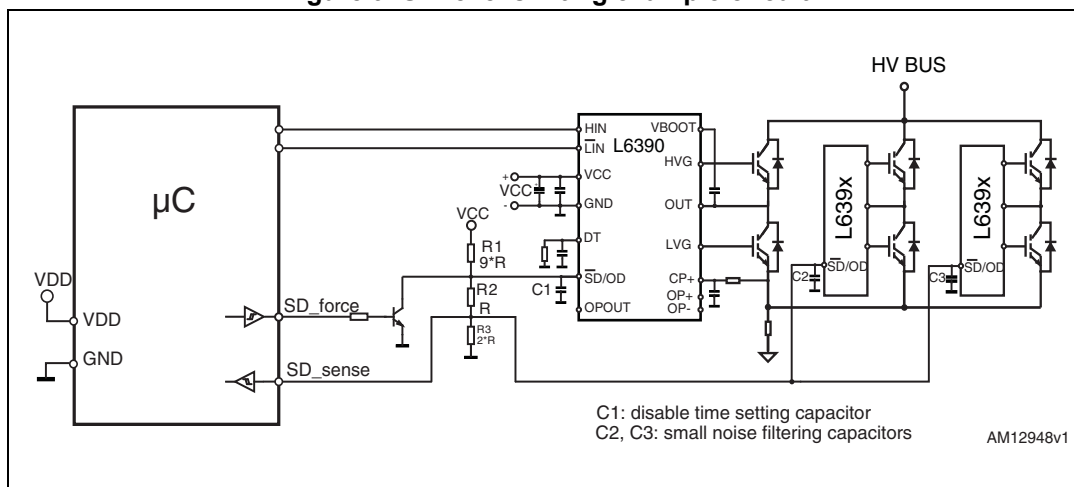
In some applications it may be useful to latch the driver in the shutdown condition for an arbitrary time, until the controller decides to reset it to normal operation. This may, for example, be achieved with a circuit similar to the one shown in Figure 8. When the open drain starts pulling down the SD/OD pin, the external latch turns on and keeps the pin to GND, preventing it from being pulled up again once the SD logic input lower threshold is reached and the internal open drain turns off. One pin of the controller is used to release the external latch, and one to externally force a shutdown condition and also to read the status of the SD/OD pin.

Figure 8. Protection latching example circuit



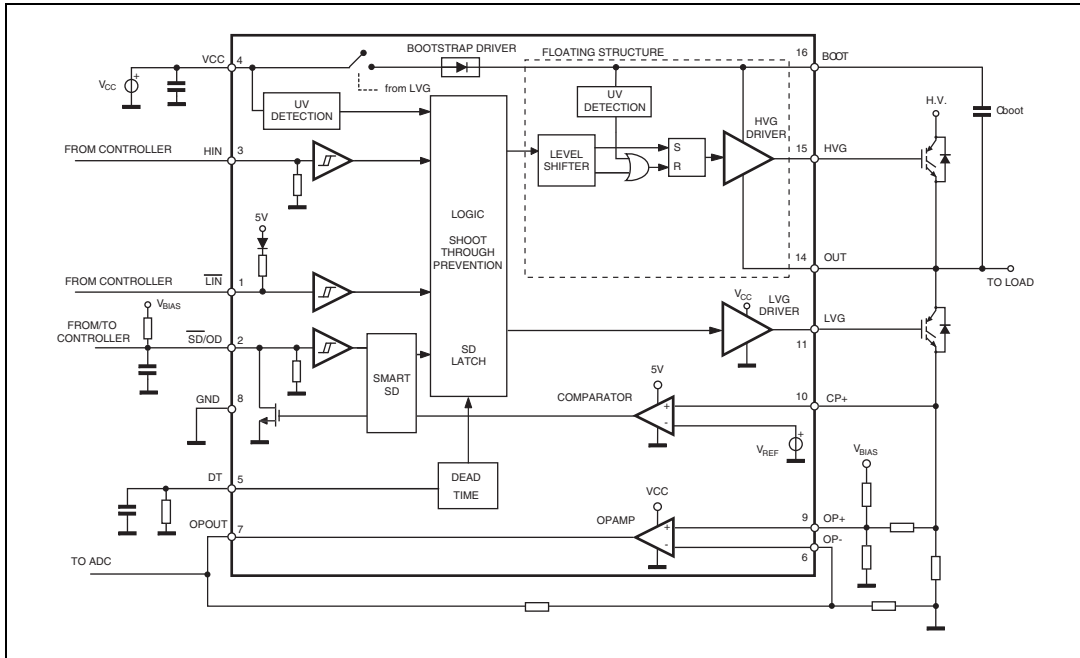
In applications using only one L6390 for the protection of several different legs (such as a single-shunt inverter, for example) it may be useful to implement the resistor divider shown in Figure 9. This simple network allows the pushing of the SD pins of the other devices to a voltage lower than L6390 V_{il} , so that each device can reach its low logic level regardless of part-to-part variations of the thresholds.

Figure 9. SD level shifting example circuit



8 Typical application diagram

Figure 10. Application diagram



9 Bootstrap driver

A bootstrap circuitry is needed to supply the high voltage section. This function is normally accomplished by a high voltage fast recovery diode (*Figure 11.a*). In the L6390 device a patented integrated structure replaces the external diode. It is realized by a high voltage DMOS, driven synchronously with the low-side driver (LVG), with a diode in series, as shown in *Figure 11.b*. An internal charge pump (*Figure 11.b*) provides the DMOS driving voltage.

C_{BOOT} selection and charging

To choose the proper C_{BOOT} value the external MOS can be seen as an equivalent capacitor. This capacitor C_{EXT} is related to the MOS total gate charge:

Equation 1

$$C_{EXT} = \frac{Q_{gate}}{V_{gate}}$$

The ratio between the capacitors C_{EXT} and C_{BOOT} is proportional to the cyclical voltage loss. It must be:

Equation 2

$$C_{BOOT} \gg \gg C_{EXT}$$

E.g.: if Q_{gate} is 30 nC and V_{gate} is 10 V, C_{EXT} is 3 nF. With $C_{BOOT} = 100$ nF the drop would be 300 mV.

If HVG must be supplied for a long time, the C_{BOOT} selection must also take the leakage and quiescent losses into account.

E.g.: HVG steady-state consumption is lower than 240 μ A, so if HVG T_{ON} is 5 ms, C_{BOOT} must supply 1.2 μ C to C_{EXT} . This charge on a 1 μ F capacitor means a voltage drop of 1.2 V.

The internal bootstrap driver offers important advantages: the external fast recovery diode can be avoided (it usually has a high leakage current).

This structure can work only if V_{OUT} is close to GND (or lower) and, at the same time, the LVG is on. The charging time (T_{charge}) of the C_{BOOT} is the time in which both conditions are fulfilled and it must be long enough to charge the capacitor.

The bootstrap driver introduces a voltage drop due to the DMOS R_{DSon} (typical value: 120 Ω). This drop can be neglected at low switching frequency, but it should be taken into account when operating at high switching frequency.

The following equation is useful to compute the drop on the bootstrap DMOS:

Equation 3

$$V_{\text{drop}} = I_{\text{charge}} R_{\text{dson}} \rightarrow V_{\text{drop}} = \frac{Q_{\text{gate}}}{T_{\text{charge}}} R_{\text{dson}}$$

where Q_{gate} is the gate charge of the external power MOSFET, R_{dson} is the on-resistance of the bootstrap DMOS and T_{charge} is the charging time of the bootstrap capacitor.

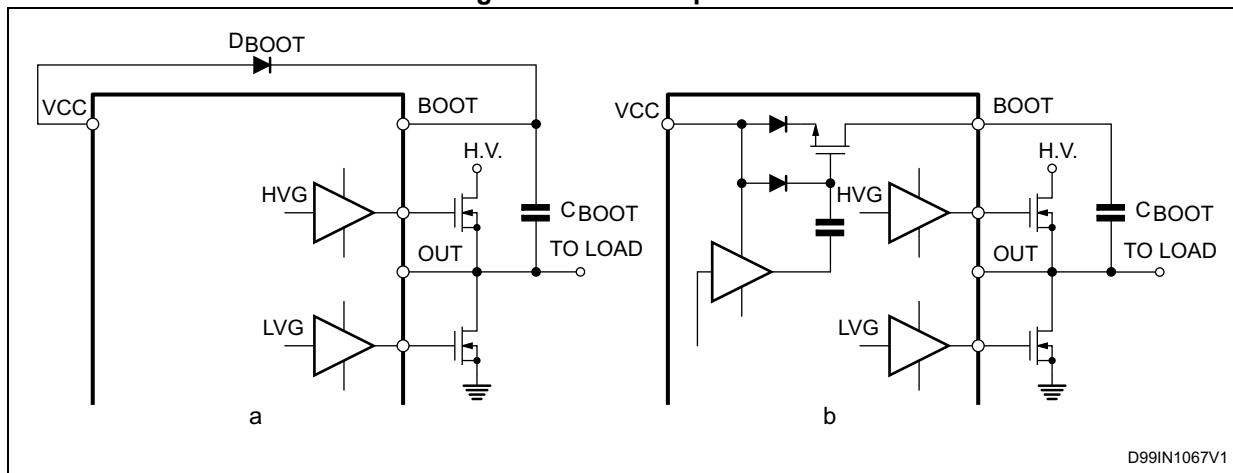
For example: using a power MOSFET with a total gate charge of 30 nC, the drop on the bootstrap DMOS is about 1 V, if the T_{charge} is 5 μs . In fact:

Equation 4

$$V_{\text{drop}} = \frac{30\text{nC}}{5\mu\text{s}} \cdot 120\Omega \sim 0.7\text{V}$$

V_{drop} should be taken into account when the voltage drop on C_{BOOT} is calculated: if this drop is too high, or the circuit topology doesn't allow a sufficient charging time, an external diode can be used.

Figure 11. Bootstrap driver



D99IN1067V1

10 Package information

In order to meet environmental requirements, ST offers these devices in different grades of ECOPACK® packages, depending on their level of environmental compliance. ECOPACK specifications, grade definitions and product status are available at: www.st.com. ECOPACK is an ST trademark.

10.1 SO-16 package information

Figure 12. SO-16 narrow package outline

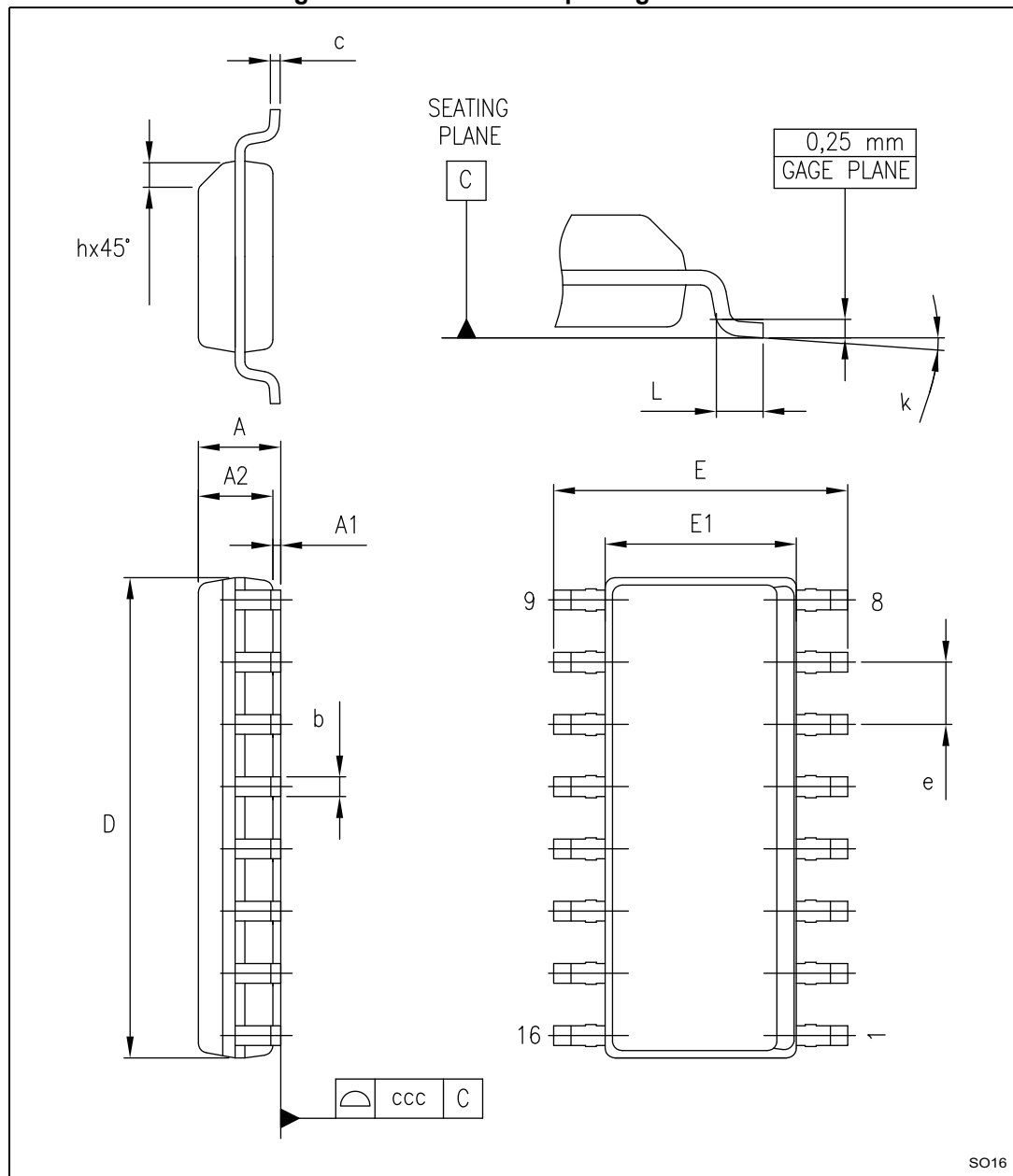
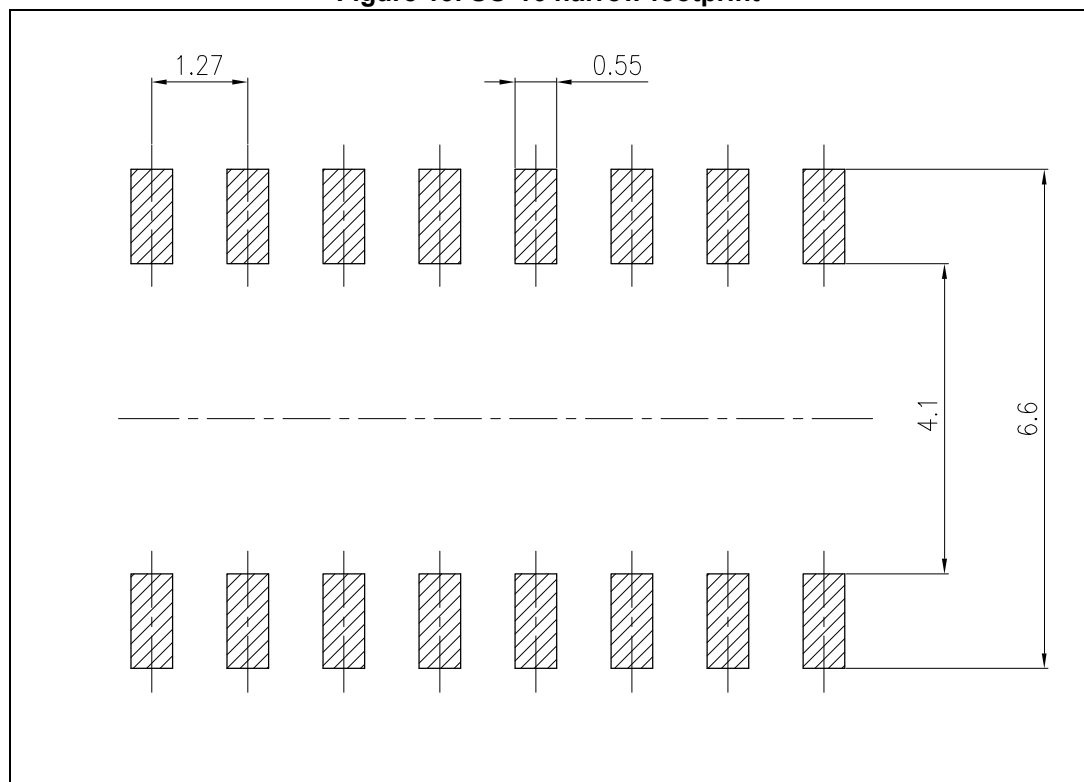


Table 10. SO-16 narrow package mechanical data

| Symbol | Dimensions (mm) | | |
|--------|-----------------|------|-------|
| | Min. | Typ. | Max. |
| A | - | - | 1.75 |
| A1 | 0.10 | - | 0.25 |
| A2 | 1.25 | - | - |
| b | 0.31 | - | 0.51 |
| c | 0.17 | - | 0.25 |
| D | 9.80 | 9.90 | 10.00 |
| E | 5.80 | 6.00 | 6.20 |
| E1 | 3.80 | 3.90 | 4.00 |
| e | - | 1.27 | - |
| h | 0.25 | - | 0.50 |
| L | 0.40 | - | 1.27 |
| k | 0 | - | 8° |
| ccc | - | - | 0.10 |

Figure 13. SO-16 narrow footprint



11 Order codes

Table 11. Order codes

| Order code | Package | Packaging |
|------------|---------|---------------|
| L6390D | SO-16 | Tube |
| L6390DTR | SO-16 | Tape and reel |

12 Revision history

Table 12. Document revision history

| Date | Revision | Changes |
|-------------|----------|--|
| 11-Sep-2015 | 9 | <p>Removed DIP-16 package from the whole document.</p> <p>Updated <i>Table 3 on page 6</i> (added ESD parameter and value).</p> <p>Updated <i>Table 4 on page 6</i> (updated $R_{th(JA)}$ value).</p> <p>Updated note 1.and 2. below <i>Table 7 on page 10</i> (minor modifications, replaced V_{CBOOTx} by V_{BOOTx}).</p> <p>Minor modifications throughout document.</p> |
| 07-Apr-2017 | 10 | <p>Updated <i>Table 5 on page 7</i> (updated cross reference to <i>Figure 4 on page 12</i> instead of removed <i>Figure 3. Timing</i>).</p> <p>Updated <i>Table 6 on page 9</i> (added R_{PD_SD}) and <i>Table 8 on page 11</i> (added R_{ON_OD}).</p> <p>Updated <i>Section 5 on page 12</i> (updated title, added <i>Figure 4</i> and <i>Figure 5</i>).</p> <p>Added <i>Section 6 on page 14</i> (and moved <i>Table 9: Truth table</i> to this section).</p> <p>Updated <i>Figure 11 on page 20</i> and <i>Figure 12 on page 21</i> (replaced by new figure).</p> <p>Minor modifications throughout document.</p> |
| 21-Mar-2018 | 11 | <p>Updated Figure of SO-16 package on page 1 and <i>Figure 2: Pin connection (top view) on page 4</i>.</p> <p>Updated <i>Table 5 on page 7</i> (updated DT and MDT test conditions).</p> <p>Updated note 2. below <i>Table 7 on page 11</i>.</p> <p>Updated <i>Section 6 on page 14</i>.</p> <p>Minor modifications throughout document.</p> |

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